### MIC23051



# 4MHz PWM Buck Regulator with HyperLight Load™ and Voltage Scaling

### **General Description**

The Micrel MIC23051 is a high efficiency 600mA PWM synchronous buck (step-down) regulator featuring HyperLight Load  $^{\text{TM}}$ , a patented switching scheme that offers best in class light load efficiency and transient performance while providing very small external components and low output ripple at all loads.

The MIC23051 has an output voltage scaling feature that can toggles between two different voltage levels.

The MIC23051 also has a very low typical quiescent current draw of  $20\mu\text{A}$  and can achieve over 85% efficiency even at 1mA. The device allows operation with a tiny inductor ranging from  $0.47\mu\text{H}$  to  $2.2\mu\text{H}$  and uses a small output capacitor that enables a sub-1mm height solution.

In contrast to traditional light load schemes HyperLight Load  $^{\text{TM}}$  architecture does not need to trade off control speed to obtain low standby currents and in doing so the device only needs a small output capacitor to absorb the load transient as the powered device goes from light load to full load.

At higher loads the MIC23051 provides a constant switching frequency of greater than 4MHz while providing peak efficiencies greater than 93%.

The MIC23051 is available in fixed output voltage options from 0.72V to 3.3V eliminating external feedback components. The MIC23051 is available in an 8-pin 2mm x 2mm MLF  $^{\tiny @}$  with a junction operating range from  $-40\,^{\circ}\text{C}$  to  $+125\,^{\circ}\text{C}$ .

Data sheets and support documentation can be found on Micrel's web site at: www.micrel.com.

### **Features**

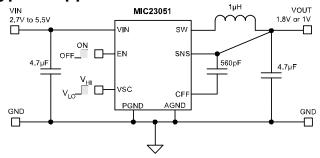


- Input voltage: 2.7V to 5.5V
- HyperLight Load™
- 600mA output current
- Fixed output voltage from 0.72V to 3.3V
- Output voltage scaling option
- Ultra fast transient response
- 20µA typical quiescent current
- 4MHz in CCM PWM operation in normal mode
- 0.47μH to 2.2μH inductor
- Low voltage output ripple
  - 25mVpp in HyperLight Load mode
  - 3mV output voltage ripple in full PWM mode
- >93% efficiency
- ~85% at 1mA
- Micropower shutdown
- Available in 8-pin 2mm x 2mm MLF<sup>®</sup>
- –40°C to +125°C junction temperature range

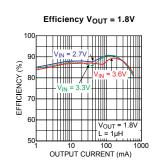
# **Applications**

- · Cellular phones
- · Digital cameras
- Portable media players
- · Wireless LAN cards
- WiFi/WiMax/WiBro modules
- USB Powered Devices

Typical Application



HyperLight Load is a trademark of Micrel, Inc. MLF and *Micro*LeadFrame are registered trademarks of Amkor Technology, Inc.



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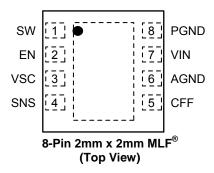
# **Ordering Information**

Part Number	Marking	Voltage Scaled to with VSC low	Nominal Output Voltage	Junction Temp. Range	Package	Lead Finish
MIC23051-CGYML	JCG	1.0V	1.8V	–40° to +125°C	8-Pin 2x2 MLF®	Pb-Free
MIC23051-C4YML	JC4	1.0V	1.2V	–40° to +125°C	8-Pin 2x2 MLF <sup>®</sup>	Pb-Free
MIC23051-16YML	J16	1.15V	1.40V	–40° to +125°C	8-Pin 2x2 MLF®	Pb-Free
MIC23051-945YML	945	0.95V	1.25V	–40° to +125°C	8-Pin 2x2 MLF®	Pb-Free

#### Note

- 1. Other output voltage combinations (0.72 to 3.3V) available, contact Micrel Marketing for details.
- 2. MLF® is a GREEN RoHS compliant package. Lead finish is NiPdAu. Mold compound is Halogen Free.

# **Pin Configuration**



# **Pin Description**

Pin Number	Pin Name	Pin Name
1	SW	Switch (Output): Internal power MOSFET output switches.
2	EN	Enable (Input). Logic low will shut down the device, reducing the quiescent current to less than $4\mu A$ . Do not leave floating.
3	VSC	Voltage scaling pin (input): A low on this pin will scale the output voltage down to specified level. Do not leave floating.
4	SNS	Connect to V <sub>OUT</sub> to sense output voltage.
5	CFF	Feed Forward Capacitor. Connect a 560pF capacitor.
6	AGND	Analog Ground.
7	VIN	Supply Voltage (Input): Requires bypass capacitor to GND.
8	PGND	Power Ground.

# **Absolute Maximum Ratings**(1)

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# Operating Ratings<sup>(2)</sup>

Supply Voltage (V <sub>IN</sub> )	2.7V to 5.5V
Logic Input Voltage (V <sub>EN)</sub>	0.3V to V <sub>IN</sub>
Junction Temperature (T <sub>J</sub> )	40°C ≤ T <sub>J</sub> ≤ +125°C
Thermal Resistance	
2x2 MLF-8 (θ <sub>JA</sub> )	90°C/W

### Electrical Characteristics<sup>(4)</sup>

 $T_A$  = 25°C with  $V_{IN}$  =  $V_{EN}$  =  $V_{SC}$  = 3.6V; L = 1 $\mu$ H;  $C_{FF}$  = 560pF;  $C_{OUT}$  = 4.7 $\mu$ F;  $I_{OUT}$  = 20mA unless otherwise specified. **Bold** values indicate  $-40^{\circ}C \le T_J \le +125^{\circ}C$ . Important design targets are in *italics*.

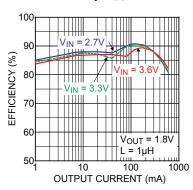
Parameter	Condition	Min	Тур	Max	Units
Supply Voltage Range		2.7		5.5	V
Under-Voltage Lockout Threshold	(turn-on)	2.45	2.55	2.65	V
UVLO Hysteresis			100		mV
Quiescent Current, Hyper LL mode	$I_{OUT} = 0mA$ , SNS > 1.8V		20	35	μΑ
Shutdown Current	$V_{IN} = 5.5V; V_{EN} = 0V;$		0.01	4	μA
Output Voltage Accuracy	VSC High, V <sub>IN</sub> = 3.0V, I <sub>LOAD</sub> = 20mA -2.			+2.5	% %
Output Voltage Accuracy	VSC Low, V <sub>IN</sub> = 3.0V, I <sub>LOAD</sub> = 20mA			+2.5	% %
SNS pin input current	V <sub>OUT</sub> = 1V		1		μA
Current Limit in PWM Mode	$SNS = 0.9*V_{NOM}$	0.65	1	1.7	Α
Output Voltage Line Regulation	$V_{IN}$ = 3.0V to 5.5V, $I_{LOAD}$ = 20mA, $V_{SC}$ = 3.6V		0.5		%
Output Voltage Load Regulation	20mA < I <sub>LOAD</sub> < 500mA, V <sub>SC</sub> = 3.6V		0.3		%
Output Voltage Line Regulation	$V_{IN}$ = 3.0V to 5.5V, $I_{LOAD}$ = 20mA, $V_{SC}$ = 0V		0.5		%
Output Voltage Load Regulation	20mA < I <sub>LOAD</sub> < 500mA, V <sub>SC</sub> = 0V		0.3		%
Maximum Duty Cycle	$SNS \le V_{NOM}, V_{OUT} = 1.8V$	80	89		%
PWM Switch ON-Resistance** See Design Note	I <sub>SW</sub> = 100mA PMOS I <sub>SW</sub> = -100mA NMOS		0.45 0.5		Ω
	V <sub>SC</sub> = 3.6V, I <sub>LOAD</sub> = 120mA	3.4	4	4.6	MHz
Frequency	V <sub>SC</sub> = 0V, I <sub>LOAD</sub> = 120mA	3.4	0.5 4 4 4.6 4 4 4.6	MHz	
SoftStart Time	V <sub>OUT</sub> = 90%		650		μs
VSC threshold voltage		0.5		1.2	V
VSC hysteresis			20		mV
Outrot transition time	VSC from low to high		800		μs
Output transition time	VSC from high to low		800		
Enable Threshold	(turn-on)	0.5		1.2	V
Enable Hysteresis			35		mV
Enable Input Current			0.1	2	μA
Over-temperature Shutdown			165		°C
Over-temperature Shutdown Hysteresis			20		°C

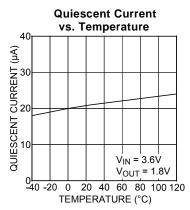
#### Notes:

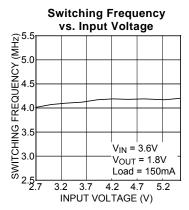
- 1. Exceeding the absolute maximum rating may damage the device.
- 2. The device is not guaranteed to function outside its operating rating.
- 3. Devices are ESD sensitive. Handling precautions recommended. Human body model,  $1.5k\Omega$  in series with 100pF.
- 4. Specification for packaged product only.

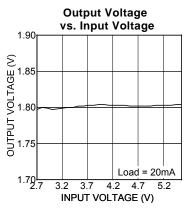
### **Typical Characteristics**

#### Efficiency Vout = 1.8V

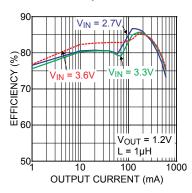


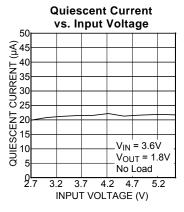


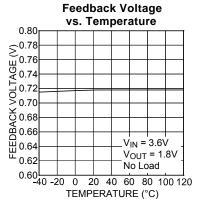


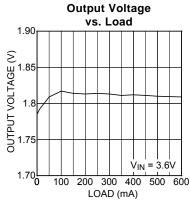


#### Efficiency Vout = 1.2V

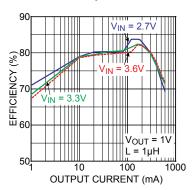


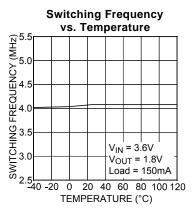


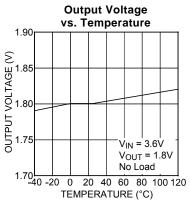




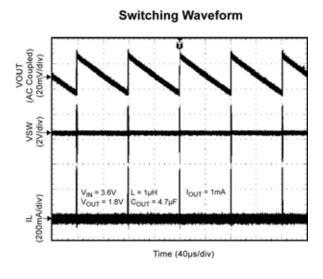
#### Efficiency Vout = 1V

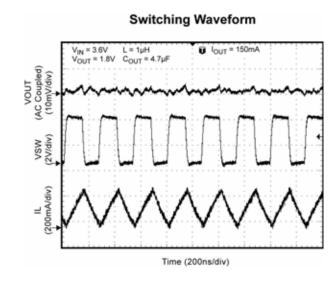


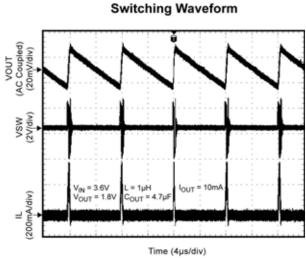


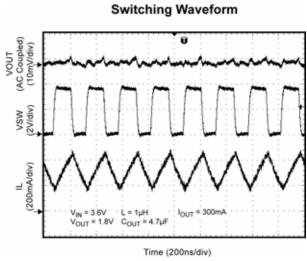


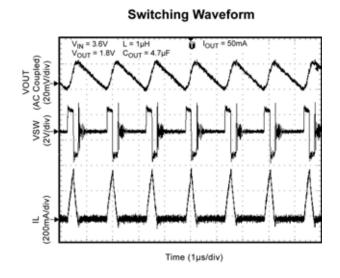
### **Functional Characteristics**

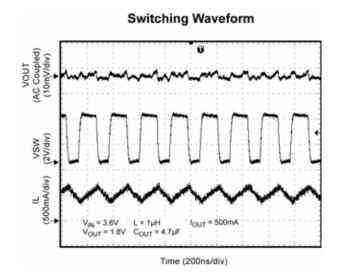




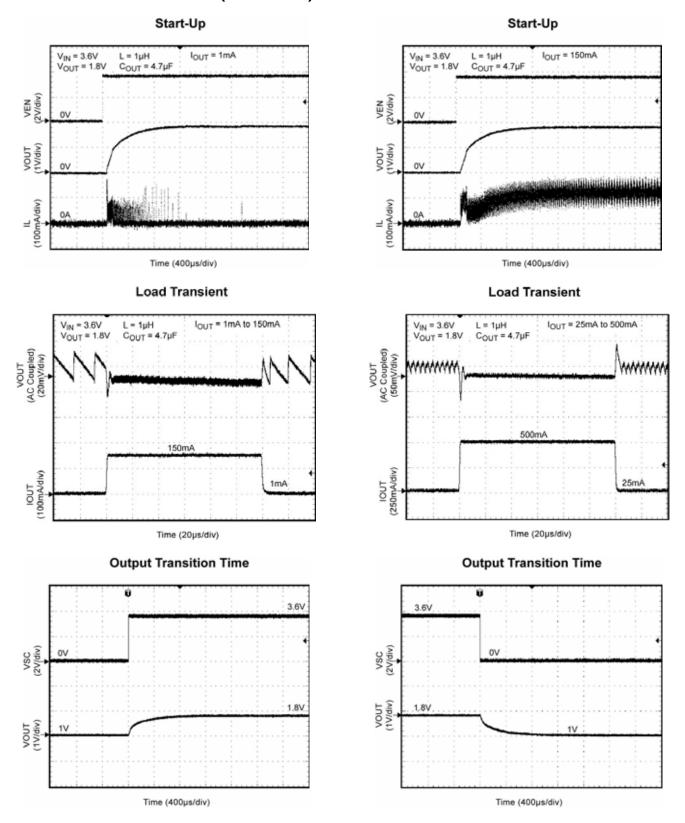




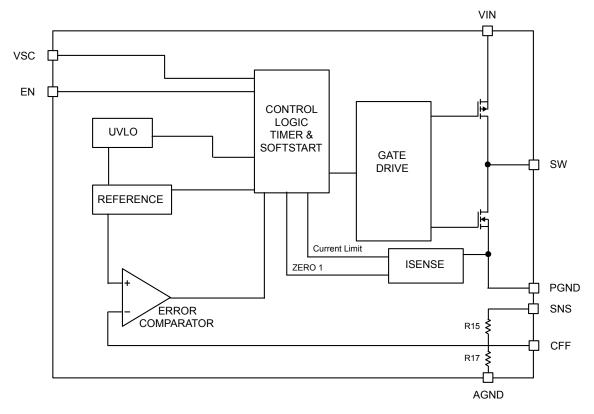




# **Functional Characteristics (continued)**



# **Functional Diagram**



MIC23051 Simplified Block Diagram

### **Functional Description**

#### VIN

VIN provides power to the MOSFETs for the switch mode regulator section and to the analog supply circuitry. Due to the high switching speeds, a  $2.2\mu F$  or greater capacitor is recommended close to VIN and the power ground (PGND) pin for bypassing. Refer to the layout recommendations for details.

#### ΕN

The enable pin (EN) controls the on and off state of the device. A logic high on the enable pin activates the regulator, while a logic low deactivates it. MIC23051 features built-in soft-start circuitry that reduces in-rush current and prevents the output voltage from overshooting at start up. Do not leave floating.

#### SW

The switch (SW) pin connects directly to the inductor and provides the switching current necessary to operate in PWM mode. Due to the high speed switching on this pin, the switch node should be routed away from sensitive nodes such as the CFF pin.

#### **SNS**

An inductor is connected from the SW pin to the SNS pin. The SNS pin is the output pin of the device and a minimum of  $2.2\mu F$  bypass capacitor should be connected in shunt. In order to reduce parasitic inductance it is good practice to place the output bypass capacitor as close to the inductor as possible.

#### **CFF**

The CFF pin is connected to the SNS pin of MIC23051 with a feed-forward capacitor of 560pF. The CFF pin itself is compared with the internal reference voltage ( $V_{REF}$ ) of the device and provides the control path to control the output.  $V_{REF}$  is equal to 0.72V. The CFF pin is sensitive to noise and should be place away from the SW pin. Refer to the layout recommendations for details.

#### **VSC**

The voltage scaling pin (VSC) is used to switch between two different voltage levels. A logic high on the VSC pin will set the output voltage to the higher voltage. A logic low on the VSC pin will set the output voltage to the lower voltage. Do not leave floating.

#### **PGND**

Power ground (PGND) is the ground path for the high current PWM mode. The current loop for the power ground should be as small as possible and separate from the Analog ground (AGND) loop. Refer to the layout recommendations for more details.

#### **AGND**

Signal ground (AGND) is the ground path for the biasing and control circuitry. The current loop for the signal ground should be separate from the Power ground (PGND) loop. Refer to the layout recommendations for more details.

### **Applications Information**

#### **Input Capacitor**

A minimum of  $2.2\mu F$  ceramic capacitor should be placed close to the VIN pin and PGND pin for bypassing. X5R or X7R dielectrics are recommended for the input capacitor. Y5V dielectrics, aside from losing most of their capacitance over temperature, they also become resistive at high frequencies. This reduces their ability to filter out high frequency noise.

#### **Output Capacitor**

The MIC23051 was designed for use with a  $2.2\mu F$  or greater ceramic output capacitor. A low equivalent series resistance (ESR) ceramic output capacitor either X7R or X5R is recommended. Y5V and Z5U dielectric capacitors, aside from the undesirable effect of their wide variation in capacitance over temperature, become resistive at high frequencies.

#### **Inductor Selection**

Inductor selection will be determined by the following (not necessarily in the order of importance);

- Inductance
- Rated current value
- Size requirements
- DC resistance (DCR)

The MIC23051 was designed for use with an inductance range from  $0.47\mu H$  to  $2.2\mu H$ . Typically, a  $1\mu H$  inductor is recommended for a balance of transient response, efficiency and output ripple. For faster transient response a  $0.47\mu H$  inductor may be used. For lower output ripple, a  $2.2\mu H$  is recommended.

Maximum current ratings of the inductor are generally given in two methods; permissible DC current and saturation current. Permissible DC current can be rated either for a 40°C temperature rise or a 10% to 20% loss in inductance. Ensure the inductor selected can handle the maximum operating current. When saturation current is specified, make sure that there is enough margin so that the peak current of the inductor does not cause it to saturate. Peak current can be calculated as follows:

$$I_{PK} = I_{OUT} + V_{OUT} (1-V_{OUT}/V_{IN})/2fL$$

As shown by the previous calculation, the peak inductor current is inversely proportional to the switching frequency and the inductance; the lower the switching frequency or the inductance the higher the peak current. As input voltage increases the peak current also increases.

The size of the inductor depends on the requirements of the application. Refer to the Application Circuit and Bill of Material for details.

DC resistance (DCR) is also important. While DCR is inversely proportional to size, DCR can represent a

significant efficiency loss. Refer to the Efficiency Considerations.

#### Compensation

The MIC23051 is designed to be stable with a  $0.47\mu H$  to  $2.2\mu H$  inductor with a  $2.2\mu F$  ceramic (X5R) output capacitor.

### **Efficiency Considerations**

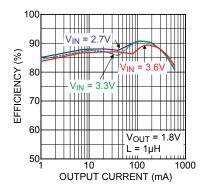
Efficiency is defined as the amount of useful output power, divided by the amount of power supplied.

$$Efficiency\_\% = \left(\frac{V_{OUT} \times I_{OUT}}{V_{IN} \times I_{IN}}\right) \times 100$$

Maintaining high efficiency serves two purposes. It reduces power dissipation in the power supply, reducing the need for heat sinks and thermal design considerations and it reduces consumption of current for battery powered applications. Reduced current draw from a battery increases the devices operating time and is critical in hand held devices.

There are two types of losses in switching converters; DC losses and switching losses. DC losses are simply the power dissipation of  $I^2R$ . Power is dissipated in the high side switch during the on cycle. Power loss is equal to the high side MOSFET  $R_{DSON}$  multiplied by the Switch Current<sup>2</sup>. During the off cycle, the low side N-channel MOSFET conducts, also dissipating power. Device operating current also reduces efficiency. The product of the quiescent (operating) current and the supply voltage is another DC loss. The current required driving the gates on and off at a constant 4MHz frequency and the switching transitions make up the switching losses.

#### Efficiency Vout = 1.8V



The Figure above shows an efficiency curve. From no load to 100mA, efficiency losses are dominated by quiescent current losses, gate drive and transition losses. By using the HyperLight Load mode the MIC23051 is able to maintain high efficiency at low output currents.

Over 100mA, efficiency loss is dominated by MOSFET  $R_{\text{DSON}}$  and inductor losses. Higher input supply voltages will increase the Gate to Source threshold on the internal

MOSFETs, reducing the internal  $R_{DSON}$ . This improves efficiency by reducing DC losses in the device. All but the inductor losses are inherent to the device. In which case, inductor selection becomes increasingly critical in efficiency calculations. As the inductors are reduced in size, the DC resistance (DCR) can become quite significant. The DCR losses can be calculated as follows;

L Pd = 
$$I_{OUT}^2 \times DCR$$

From that, the loss in efficiency due to inductor resistance can be calculated as follows:

$$Efficiency\_Loss = \left[1 - \left(\frac{V_{OUT} \times I_{OUT}}{V_{OUT} \times I_{OUT} + L\_Pd}\right)\right] \times 100$$

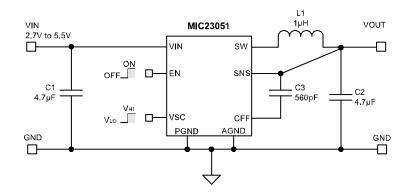
Efficiency loss due to DCR is minimal at light loads and gains significance as the load is increased. Inductor selection becomes a trade-off between efficiency and size in this case.

#### HyperLight Load Mode™

MIC23051 uses a minimum on and off time proprietary control loop. When the output voltage falls below the regulation threshold, the error comparator begins a switching cycle that turns the PMOS on and keeps it on for the duration of the minimum-on-time. When the output voltage is over the regulation threshold, the error comparator turns the PMOS off for a minimum-off-time. The NMOS acts as an ideal rectifier that conducts when the PMOS is off. Using a NMOS switch instead of a diode allows for lower voltage drop across the switching device when it is on. The asynchronous switching combination between the PMOS and the NMOS allows the control loop to work in discontinuous mode for light load operations. In discontinuous mode MIC23051 works in pulse frequency modulation (PFM) to regulate the output. As the output current increases, the switching frequency increases. This improves the efficiency of MIC23051 during light load currents. As the load current increases, the MIC23051 goes into continuous conduction mode (CCM) at a constant frequency of 4MHz. The equation to calculate the load when the MIC23051 goes into continuous conduction mode may be approximated by the following formula:

$$I_{LOAD} = \left(\frac{(V_{IN} - V_{OUT}) \times D}{2L \times f}\right)$$

# **MIC23051 Typical Application Circuit**



# **Bill of Materials**

Item	Part Number	Manufacturer	Description	Qty	
C1, C2	C1608X5R0J476K	TDK <sup>(1)</sup>	4.7μF Ceramic Capacitor, 6.3V, X5R, Size 0603	2	
C3	C1608C0G1H561J	TDK <sup>(1)</sup>	560pF Ceramic Capacitor, 50V, NPO, Size 0603	1	
L1	LQM21PN1R0MC0D	Murata <sup>(2)</sup>	1μH, 0.8A, 190mΩ, L2mm x W1.25mm x H0.5mm		
	LQH32CN1R0M33	Murata <sup>(2)</sup>	1μH, 1A, 60mΩ, L3.2mm x W2.5mm x H2.0mm		
	LQM31PN1R0M00	Murata <sup>(2)</sup>	1μH, 1.2A, 120mΩ, L3.2mm x W1.6mm x H0.95mm	1	
	CPL2512T1R0M	TDK <sup>(1)</sup>	1μH, 1.5A, 100mΩ, L2.5mm x W1.5mm x H1.2mm	] '	
	LQM31PNR47M00	Murata <sup>(2)</sup>	0.47μH, 1.4A, 80mΩ, L3.2mm x W1.6mm x H0.85mm		
	MIPF2520D1R5	FDK <sup>(3)</sup>	1.5μH, 1.5A, 70mΩ, L2.5mm x W2mm x H1.0mm		
U1	MIC23051-xxYML	Micrel, Inc. (4)	4MHz PWM Buck Regulator with HyperLight Load Mode		

#### Notes:

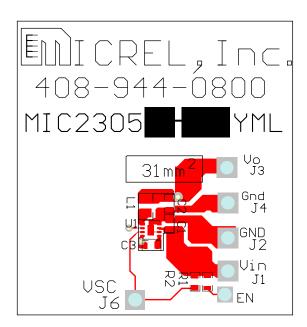
1. TDK: www.tdk.com

2. Murata: www.murata.com

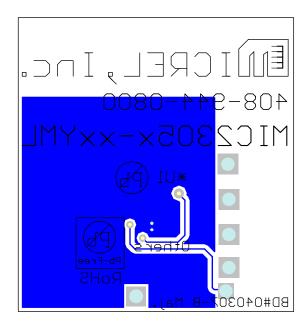
3. FDK: www.fdk.co.jp

4. Micrel, Inc: www.micrel.com

# **PCB Layout Recommendations**

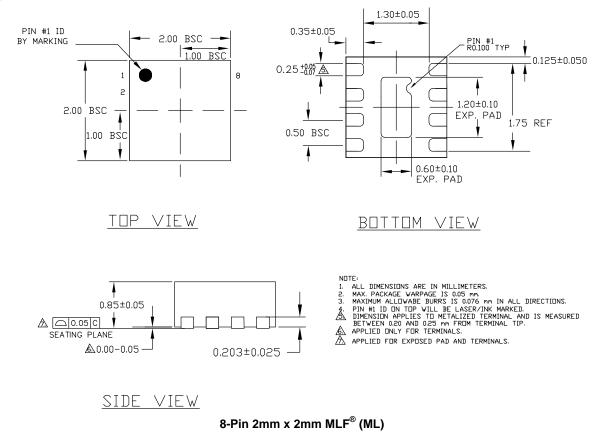


**Top Layer** 



**Bottom Layer** 

### **Package Information**



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